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II. Envelope Equations

Paraxial Ray Equation

Envelope equations for axially
symmetric beams

Cartesian equation of motion

Envelope equations for elliptically
symmetric beams

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Roadmap:

Single particle equation with Lorentz force
 $q(E + v \times B)$



Make use of:

1. Paraxial (near-axis) approximation
(Small r and r')
2. Conservation of canonical angular momentum
3. Axisymmetry $f(r,z)$



Paraxial Ray Equation for Single Particle

Next take statistical averages over the distribution function

⇒ Moment equations

Express some of the moments in terms of the rms radius and emittance

⇒ Envelope equations (axi-symmetric case)

Some focusing systems have quadrupolar symmetry
Rederive envelope equations in cartesian coordinates
(x,y,z) rather than radial (r,z)

J. BARNARD (3)

START WITH NEWTON'S EQUATION WITH THE LORENTZ FORCE:

$$\frac{d\mathbf{F}}{dt} = q(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

In cartesian coordinates:

$$\frac{d}{dt}(mv_x) = \gamma m \dot{x} + \gamma m \ddot{x} = q(E_x + \dot{y}B_z - \dot{z}B_y)$$

$$\frac{d}{dt}(mv_y) = \gamma m \dot{y} + \gamma m \ddot{y} = q(E_y + \dot{z}B_x - \dot{x}B_z)$$

$$\frac{d}{dt}(mv_z) = \gamma m \dot{z} + \gamma m \ddot{z} = q(E_z + \dot{x}B_y - \dot{y}B_x)$$

In cylindrical coordinates: (use $\frac{d\hat{\mathbf{r}}}{dt} = \hat{\mathbf{e}}_\theta \dot{\theta}$; $\frac{d\hat{\mathbf{e}}_\theta}{dt} = -\hat{\mathbf{e}}_r \dot{\theta}$)
(see next page)

$$\frac{d}{dt}(mv_r) - \gamma m r^2 \dot{\theta}^2 = q(E_r + r\dot{\theta}B_z - zB_\theta) \quad (\text{I})$$

$$\frac{1}{r} \frac{d}{dt}(mv_r^2 \dot{\theta}) = q(E_\theta + \dot{z}B_r - \dot{r}B_z) \quad (\text{II})$$

$$\frac{d}{dt}(mv_z) = q(E_z + \dot{r}B_\theta - r\dot{\theta}B_r) \quad (\text{III})$$

When $\frac{\partial}{\partial \theta} = 0$:

$$\mathbf{E} = -\nabla \phi - \frac{\partial \mathbf{A}}{\partial t} = \hat{\mathbf{e}}_r \left[-\frac{\partial \phi}{\partial r} - \frac{\partial A_r}{\partial t} \right] + \hat{\mathbf{e}}_\theta \left[-\frac{\partial \phi}{\partial \theta} \right] + \hat{\mathbf{e}}_z \left[-\frac{\partial \phi}{\partial z} - \frac{\partial A_z}{\partial t} \right]$$

$$\mathbf{B} = \nabla \times \mathbf{A} = \hat{\mathbf{e}}_r \left[-\frac{\partial}{\partial z} A_\theta \right] + \hat{\mathbf{e}}_\theta \left[\frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right] + \hat{\mathbf{e}}_z \left[\frac{1}{r} \frac{\partial}{\partial r} (r A_\theta) \right]$$

RHS of II multiplied by r :

$$\begin{aligned} qr(E_\theta + zB_r - rB_z) &= q \left(-\frac{\partial r A_\theta}{\partial t} - \dot{z} \frac{\partial r A_\theta}{\partial z} - \dot{r} \frac{\partial (r A_\theta)}{\partial r} \right) \\ &= -q \left[\frac{\partial}{\partial t} + \dot{r} \frac{\partial}{\partial r} \right] (r A_\theta) \\ &= -q \frac{d(r A_\theta)}{dt} \end{aligned} \quad (\text{IV})$$

$$\text{Eqtn II} \Rightarrow \frac{d}{dt} (-\gamma m r^2 \dot{\theta} + qr A_\theta) = 0$$

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To calculate the rate of change of the momentum \underline{p} in cylindrical coordinates, we must take into account that the unit vector changes direction as the particle moves:

LET

$$\underline{p} = p_r \hat{e}_r + p_\theta^* \hat{e}_\theta + p_z \hat{e}_z = \gamma m \underline{v}$$

where

$$p_r = \gamma m r \dot{\phi}$$

$$p_\theta^* = \gamma m r \dot{\phi}$$

$$p_z = \gamma m z$$

NOTE: ON THIS PAGE p_θ^* = θ -component of mechanical momentum
NOT TO BE CONFUSED WITH $\dot{\theta} = \gamma m r^2 \dot{\phi} + q r A \phi = \theta$ -component of CANONICAL ANGULAR momentum

$$\text{So } \frac{d\underline{p}}{dt} = \dot{p}_r \hat{e}_r + p_r \dot{\hat{e}}_r + \dot{p}_\theta^* \hat{e}_\theta + p_\theta^* \dot{\hat{e}}_\theta + \dot{p}_z \hat{e}_z$$

$$\Rightarrow \frac{d\underline{p}}{dt} = (\dot{p}_r - p_\theta^* \dot{\phi}) \hat{e}_r + (p_r \dot{\phi} + \dot{p}_\theta^*) \hat{e}_\theta + \dot{p}_z \hat{e}_z$$

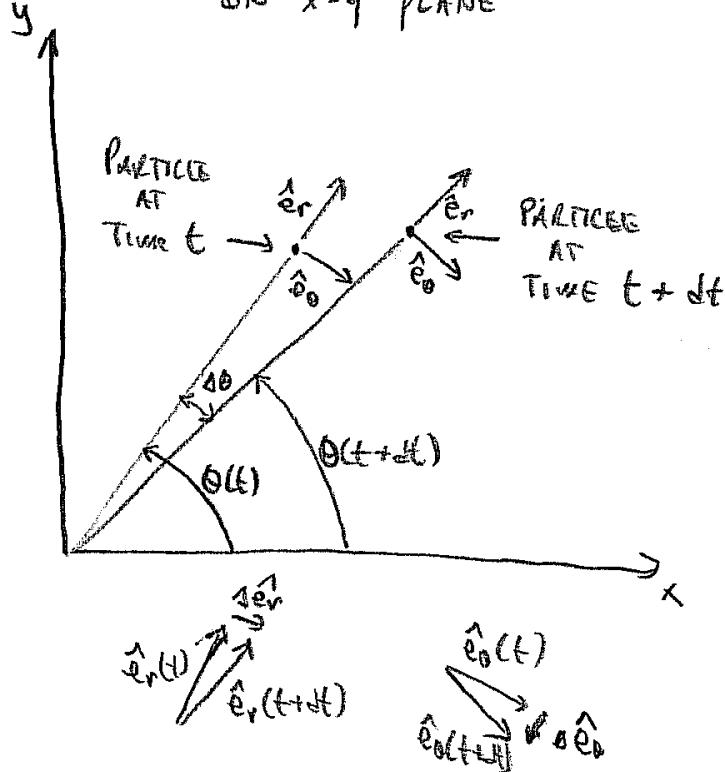
WHERE WE HAVE USED:

$$\frac{d\hat{e}_r}{dt} = \hat{e}_\theta \dot{\phi} \quad \frac{d\hat{e}_\theta}{dt} = -\hat{e}_r \dot{\phi}$$

$$\begin{aligned} \Rightarrow \frac{d\underline{p}}{dt} &= \left[\frac{d}{dt}(\gamma m r) - (\gamma m r \dot{\phi}^2) \right] \hat{e}_r \\ &+ \left[\gamma m r \dot{\phi} + \frac{d}{dt}(\gamma m \dot{\phi}) \right] \hat{e}_\theta + \frac{d}{dt}(\gamma m \dot{z}) \hat{e}_z \\ &\underbrace{= \frac{d}{dt}(\gamma m r^2 \dot{\phi})}_{\text{MECHANICAL ANGULAR MOMENTUM}} \end{aligned}$$

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PROJECTION OF PARTICLE POSITION AT TIMES t & $t+dt$
ON X-Y PLANE



$$\Delta \hat{e}_r = \hat{e}_\theta \Delta \theta \quad \Delta \hat{e}_\theta = -\hat{e}_r \Delta \theta$$

$$\frac{d \hat{e}_r}{dt} = \hat{e}_\theta \dot{\theta} \quad \frac{d \hat{e}_\theta}{dt} = -\hat{e}_r \dot{\theta}$$

CONSERVATION OF CANONICAL ANGULAR MOMENTUM

J. BAHADUR (6)

DEFINE $P_\theta = Ymr^2\dot{\theta} + qrA_\theta$

$$\frac{d}{dt} P_\theta = 0$$

(CONSERVATION OF
CANONICAL ANGULAR MOMENTUM)

NOTE THAT THE FLUX ENCLOSED BY A CIRCLE OF RADIUS r

$$\Psi = \oint \underline{B} \cdot d\underline{l} = \int (\nabla \times \underline{A}) \cdot d\underline{l} = \int \underline{A} \cdot d\underline{l} = 2\pi r A_\theta$$

$$P_\theta = Ymr^2\dot{\theta} + \frac{q\Psi}{2\pi}$$

IS CONSERVED ALONG AN ORBIT
IN AXISYMMETRICAL GEOMETRIES

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"EXTERNAL" ELECTRIC & MAGNETIC FIELD WITH

AZIMUTHAL SYMMETRY ($\frac{\partial \phi}{\partial \theta} = 0$) (REFER SECTION 5.3)

CONSIDER THE FIELD E_{ext} & B_{ext} CREATED BY EXTERNAL SOURCES:
(TIME STEADY, VACUUM FIELDS):

$$\nabla \times \underline{B}_{ext} = 0 \quad \nabla \times \underline{E}_{ext} = 0 \quad (\Rightarrow E, B \sim \nabla \phi) \\ \nabla \cdot \underline{B}_{ext} = 0 \quad \nabla \cdot \underline{E}_{ext} = 0 \quad \Rightarrow \quad \nabla^2 \phi = 0$$

In cylindrical coordinates:

$$\nabla^2 \phi = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \phi}{\partial r} \right) + \frac{\partial^2 \phi}{\partial z^2}$$

$$\text{Let } \Phi(r, z) = \sum_{v=0}^{\infty} f_{2v}(z) r^{2v} = f_0 + f_2 r^2 + f_4 r^4 + \dots$$

$$\nabla^2 \phi = 0 \quad \Rightarrow \quad \sum_{v=1}^{\infty} (2v)^2 f_{2v} r^{2v-2} + \sum_{v=0}^{\infty} f''_{2v} r^{2v} = 0$$

$$\Rightarrow f''_0(z) = -4f_2$$

$$f''_2(z) = -16f_4 \quad \Rightarrow \quad f_{2v} = \frac{(-1)^v}{(v!)^2 z^{2v}} \frac{\partial^v f(0)}{\partial z^v}$$

$$f''_4(z) = -36f_6$$

$$\Rightarrow \Phi(r, z) = \sum_{v=0}^{\infty} \frac{(-1)^v}{(v!)^2} \frac{\partial^v f(0)}{\partial z^v} \left(\frac{r}{z} \right)^{2v} = f_0(z) - \frac{1}{4} f''_0(z) r^2 \\ + \frac{1}{64} f''''_0(z) r^4 + \dots$$

Let $B_z(0, z) = B(z)$ & let $\Psi(0, z) = V(z) = f_0(z)$

$$B_z(r, z) = -\frac{\partial \phi(r, z)}{\partial z} = f'_0(z) - \frac{1}{4} f''_0(z) r^2 + \frac{1}{64} f''''_0(z) r^4 + \dots \\ = B(z) - \frac{r^2}{4} \frac{\partial^2 B(z)}{\partial z^2} + \frac{r^4}{64} \frac{\partial^4 B(z)}{\partial z^4} + \dots$$

$$B_r(r, z) = \frac{-\partial \phi(r, z)}{\partial r} = -\frac{r}{2} \frac{\partial B(z)}{\partial z} + \frac{r^3}{16} \frac{\partial^3 B(z)}{\partial z^3} + \dots$$

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Similarly, for the electric field define

$$V(z) = \Phi(0, z) = f_0(z)$$

$$\Rightarrow \Phi(r, z) = V(z) - \frac{r^2}{4} V''(z) + \frac{r^4}{64} \frac{\partial^4 V}{\partial z^4} + \dots$$

$$\Rightarrow E_r(r, z) = \frac{r}{2} V''(z) - \frac{r^3}{16} \frac{\partial^4 V(z)}{\partial z^4} + \dots$$

$$\nabla E_z(r, z) = -V'(z) + \frac{r^2}{4} V'''(z) + \dots$$

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RETURNING TO THE RADIAL COMPONENT OF THE
MOMENTUM EQUATION IN CYLINDRICAL COORDINATES (EQ I):

$$\frac{d}{dt}(\gamma mr) - \gamma mr\dot{\theta}^2 = q(E_r + r\dot{\theta}B_z - \dot{z}B_\theta) \quad (I)$$

for the external field use

$$E_{r,\text{ext}} = \frac{r}{z} V'' + O(r^3)$$

$$B_{z,\text{ext}} = B_z(z) + O(r^3)$$

$$B_{\theta,\text{ext}} = 0 \quad [\text{since } \frac{\partial \Phi_{\text{ext}}}{\partial \theta} = 0]$$

WE LET:

$$\underline{B} = \underline{B}_{\text{ext}} + \underline{B}_{\text{self}}$$

$$\underline{E} = \underline{E}_{\text{ext}} + \underline{E}_{\text{self}}$$

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PARAXIAL RAY EQUATION

$$(I) \Rightarrow \frac{d}{dt} (\gamma_m r) - \gamma_m r \dot{\theta}^2 = q \left(\frac{v''}{2} r + r \dot{\theta}' B \right) + q \left(E_r^{\text{self}} - v_z B_0^{\text{self}} \right)$$

↑ ↑ ↑ ↑ ↑ ↑
 INERTIAL CENTRIFUGAL E_r
 external external $v_z B_z$
 external external SELF
 FIELDS

Now use s as independent variable $v_z dt = ds$

$$v_z \frac{d}{ds} (\gamma_m v_z r') - \gamma_m v_z^2 r \dot{\theta}'^2 = q \left(\frac{v''}{2} r + r v_z \dot{\theta}' B \right) + q \left(E_r^{\text{self}} - v_z B_0^{\text{self}} \right)$$

EXPANDING 1st term and $v_z \approx v$; AND DIVIDING BY $\gamma_m v^2$:

$$r'' - r \dot{\theta}'^2 + \frac{v'}{c} r' = \frac{q}{\gamma_m p c^2} \left(\frac{v''}{2} r + r p c \dot{\theta}' B + E_r^{\text{self}} - v_z B_0^{\text{self}} \right) \quad (P1)$$

Using CANONICAL MOMENTUM, eliminate $\dot{\theta}'$ via

$$\dot{\theta}' = \frac{p_0 - \frac{q\psi}{2\pi}}{\gamma_m r^2 p c} = \frac{p_0}{\gamma_m r^2 p c} - \frac{qB}{2\gamma_m p c} = \frac{p_0}{\gamma_m r^2 p c} - \frac{w_c}{2\gamma_m p c}$$

where we define $w_c = \frac{qB}{m}$.

ADDING THE TWO $\dot{\theta}'$ TERMS IN THE EQUATION (P1)

$$\begin{aligned}
 -r \dot{\theta}'^2 - \frac{r w_c \dot{\theta}'}{\gamma_m p c} &= \frac{-p_0^2}{\gamma^2 m^2 r^3 p^2 c^2} + \frac{p_0 w_c}{\gamma^2 m^2 p^2 c^2 r} - \frac{r w_c^2}{4 \gamma^2 p^2 c^2} \\
 &\quad - \frac{p_0 w_c}{\gamma^2 m^2 p^2 c^2 r} + \frac{r w_c^2}{2 \gamma^2 p^2 c^2} \\
 &= \frac{-p_0^2}{\gamma^2 m^2 r^3 p^2 c^2} + \frac{r w_c^2}{2 \gamma^2 p^2 c^2}
 \end{aligned}$$

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So equation (P1) becomes:

$$r'' + \frac{\gamma'}{\gamma} r' = \frac{q}{\gamma m \beta^2 c^2} \left(\frac{V''}{2} r \right) + \frac{r \omega_c^2}{2 \gamma^2 \beta^2 c^2} + \frac{p_0^2}{\gamma^2 m v_z^2 \beta^2 c^2} + \frac{q}{\gamma m \beta^2 c^2} [E_r^{\text{self}} - V_z B_0^{\text{self}}] \quad (\text{P2})$$

$$\text{Now } \gamma' m c^2 = q \frac{E_z v_z}{V_z} \Rightarrow \gamma'' = \left(V'' + \frac{\partial^2 \phi^{\text{self}}}{\partial z^2} \right) \frac{q}{m c^2}$$

$$\text{CALCULATING } \frac{q}{\gamma m \beta^2 c^2} \left[\frac{V''}{2} r + E_r^{\text{self}} - V_z B_0^{\text{self}} \right]:$$

$$\nabla^2 \phi^{\text{self}} = -\frac{p}{\epsilon_0} \Rightarrow \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \phi}{\partial r} \right) = -\frac{p}{\epsilon_0} - \frac{\partial^2 \phi^{\text{self}}}{\partial z^2}$$

$$\Rightarrow \frac{1}{r} \left(r \frac{\partial \phi}{\partial r} \right) = -\frac{p(r)}{\epsilon_0} - \frac{r \partial^2 \phi^{\text{self}}}{\partial z^2}$$

$$r \frac{\partial \phi}{\partial r} = -\frac{1}{2\pi\epsilon_0} \int_0^r 2\pi r J_z(r) dr - \frac{r^2}{2} \frac{\partial^2 \phi}{\partial z^2}$$

$$= -\frac{1}{2\pi\epsilon_0} \lambda(r) - \frac{r^2}{2} \frac{\partial^2 \phi^{\text{self}}}{\partial z^2}$$

$$\Rightarrow E_r^{\text{self}} = \frac{\lambda(r)}{2\pi\epsilon_0 r} + \frac{r}{2} \frac{\partial^2 \phi^{\text{self}}}{\partial z^2}$$

$$\nabla \times \underline{B} = \mu_0 \underline{J} \Rightarrow 2\pi r B_0 = \mu_0 \int_0^r 2\pi r J_z(r) dr = \mu_0 V_z \lambda(r)$$

$$B_0^{\text{self}} = \frac{\mu_0 V_z \lambda(r)}{2\pi\epsilon_0 r} = \frac{V_z}{c^2} \frac{\lambda(r)}{2\pi\epsilon_0 r}$$

$$\left[\frac{V''}{2} r + E_r^{\text{self}} - V_z B_0^{\text{self}} \right] = \underbrace{\left[\frac{r}{2} \left(V'' + \frac{\partial^2 \phi^{\text{self}}}{\partial z^2} \right) + \left(1 - \frac{V_z^2}{c^2} \right) \frac{\lambda(r)}{2\pi\epsilon_0 r} \right]}_{-\frac{mc^2}{q} V''} + \frac{1}{r^2}$$

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So equation (P2) becomes: "THE PARAXIAL RAY EQUATION:"

$$r'' + \frac{\gamma' r'}{\beta^2 \gamma} + \frac{\gamma''}{z \beta^2 \gamma} r + \left(\frac{\omega_c}{z \gamma \beta c} \right)^2 r - \left(\frac{p_0}{\gamma \beta m c} \right)^2 \frac{1}{r^3} - \frac{q}{\gamma^3 m v_z^2} \frac{\lambda(r)}{z \beta \epsilon_0 r} = 0$$

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INERTIAL E_r $v_b B_z$ CENTRIFUGAL SELF
 (CONVERGENCE OF FIELD LINES)

MOMENT EQUATIONS

$$\text{Vlasov eqtn: } \frac{\partial f}{\partial s} + x' \frac{\partial f}{\partial x} + x'' \frac{\partial f}{\partial x'} + y' \frac{\partial f}{\partial y} + y'' \frac{\partial f}{\partial y'} = 0$$

$$\text{Let } g = g(x, x', y, y') ; \quad N = \iiint f dx dx' dy dy'$$

Multiply Vlasov equation by $g + \frac{1}{N} \iiint dx dx' dy dy'$

$$\int dx dx' dy dy' \left[g \frac{\partial f}{\partial s} + g x' \frac{\partial f}{\partial x} + g x'' \frac{\partial f}{\partial x'} + g y' \frac{\partial f}{\partial y} + g y'' \frac{\partial f}{\partial y'} \right] = 0$$

$$\begin{aligned} \frac{d}{ds} \underbrace{\langle g \rangle}_{\rightarrow 0} + \underbrace{\int_{x=-\infty}^{\infty} g f dx'}_{= \langle x' \frac{\partial g}{\partial x} \rangle} - \underbrace{\int_N \iiint \frac{\partial g}{\partial x} f dx'}_{= \langle x' \frac{\partial g}{\partial x} \rangle} + \dots &= 0 \end{aligned}$$

$$\Rightarrow \frac{d}{ds} \langle g \rangle = \langle x' \frac{\partial g}{\partial x} \rangle + \langle x'' \frac{\partial g}{\partial x'} \rangle + \langle y' \frac{\partial g}{\partial y} \rangle + \langle y'' \frac{\partial g}{\partial y'} \rangle$$

$$\text{But } \frac{dg}{ds} = \frac{\partial g}{\partial x} x' + \frac{\partial g}{\partial x'} x'' + \frac{\partial g}{\partial y} y' + \frac{\partial g}{\partial y'} y''$$

$$\Rightarrow \frac{d}{ds} \langle g \rangle = \langle g' \rangle$$

$$\text{So } \frac{d}{ds} \langle x^2 \rangle = 2 \langle xx' \rangle$$

$$\frac{d}{ds} \langle x'^2 \rangle = 2 \langle x' x'' \rangle \quad \text{etc...}$$

$$\frac{d}{ds} \langle xx' \rangle = \langle xx'' \rangle + \langle x'^2 \rangle$$

ENVELOPE EQUATION FOR AXISYMMETRIC BEAMS

LET $r_b^2 = 2\langle r^2 \rangle = 2(\langle x^2 \rangle + \langle y^2 \rangle) = 4\langle x^2 \rangle$
 for an
 axisymmetric
 beam

$$2r_b r_b' = 4\langle rr' \rangle \Rightarrow r_b' = \frac{2\langle rr' \rangle}{r_b}$$

$$\begin{aligned} r_b'' &= \frac{2\langle rr'' \rangle + 2\langle r'^2 \rangle}{r_b} - \frac{2\langle rr' \rangle}{r_b^2} \left(\frac{2\langle rr' \rangle}{r_b} \right) \\ &= 2 \frac{\langle rr'' \rangle}{r_b} + \frac{4\langle r^2 \rangle \langle r'^2 \rangle - 4\langle rr' \rangle^2}{r_b^3} \end{aligned}$$

WHAT IS $\langle rr'' \rangle$?

RECALL EQUATION P1 (ON PATH TO DERIVING LAY EQUATION):

$$r'' - r\theta'^2 + \frac{\gamma'}{\rho^2 \gamma} r' = \frac{q}{\gamma m \rho^2 c^2} \left(\frac{V''}{2} r + r_p c \theta' B + \epsilon_r^{\text{soft}} - V_B^{\text{soft}} \right)$$

P1 may be rewritten:

$$r'' - r\theta'^2 + \frac{\gamma'}{\rho^2 \gamma} r' = \frac{q}{\gamma m \rho^2 c^2} \left[-\frac{mc^2}{q} \gamma'' r + \frac{\lambda(r)}{\gamma^2 2kE_0 r} + r_p c \theta' B \right]$$

$$\boxed{r'' + \frac{\gamma'}{\rho^2 \gamma} r' + \frac{\gamma''}{2\rho^2 \gamma} r - \frac{q}{\gamma^3 m v_e^2} \frac{\lambda(r)}{2kE_0 r} - \frac{\omega_c}{\gamma \rho c} \theta' r - r\theta'^2 = 0}$$

What is $\langle rr'' \rangle$?

$$\langle rr'' \rangle + \frac{-\omega_c}{\gamma \rho c} \langle \theta' r^2 \rangle - \langle r^2 \theta'^2 \rangle + \dots = 0$$

$$\langle p_\theta \rangle^2 = \gamma^2 m^2 \rho^2 c^2 \langle p^2 \theta' \rangle^2 + \frac{\omega_c^2}{4} m^2 \langle r^2 \rangle^2 + \omega_c \gamma m^2 \rho c \langle r \theta' \rangle \langle r'' \rangle$$

$$\Rightarrow \frac{-\omega_c}{\gamma \rho c} \langle \theta' r^2 \rangle = \frac{-\omega_c}{\gamma \rho c} \left[\frac{\langle p_\theta \rangle^2}{\omega_c \gamma m^2 \rho c \langle r^2 \rangle} - \frac{\omega_c \langle r^2 \rangle}{4 \gamma \rho c} - \frac{\rho c \langle r^2 \theta' \rangle^2}{\omega_c \langle r^2 \rangle} \right]$$

$$\Rightarrow \langle rr'' \rangle = \frac{\langle p_\theta \rangle^2}{\gamma^2 m^2 \rho^2 c^2 \langle r^2 \rangle} + \frac{\omega_c^2 \langle r^2 \rangle}{4 \gamma^2 \rho^2 c^2} - \frac{\langle r^2 \theta' \rangle^2}{\langle r^2 \rangle} + \langle r^2 \theta'^2 \rangle + \dots = 0$$

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$$\langle rr'' \rangle = \frac{\gamma'}{\beta^2 \gamma} \langle rr' \rangle + \frac{\gamma''}{2\beta^2 \gamma} \langle r^2 \rangle - \frac{q}{\gamma^3 m V_0^2} \frac{\langle \lambda(r) \rangle}{2\pi E_0} +$$

$$\frac{\langle p_\theta \rangle^2}{(\gamma m p c)^2 \langle r^2 \rangle} - \frac{\omega_c^2 \langle r^2 \rangle}{4(\gamma p c)^2} - \frac{\langle r^2 \theta' \rangle^2}{\langle r^2 \rangle} + \langle r^2 \theta'^2 \rangle$$

$$r_b'' = \frac{2 \langle rr'' \rangle}{r_b} + \frac{4 \langle r^2 \rangle \langle r'^2 \rangle - 4 \langle rr' \rangle}{r_b^3}$$

$$= \frac{\gamma'}{\beta^2 \gamma} \frac{2 \langle rr' \rangle}{r_b} + \frac{\gamma''}{2\beta^2 \gamma} \frac{2 \langle r^2 \rangle}{r_b} - \frac{2q}{\gamma^3 m V_0^2} \frac{\langle \lambda(r) \rangle}{2\pi E_0} \frac{1}{r_b}$$

$$+ \frac{\langle p_\theta \rangle^2}{(\gamma m p c)^2} \frac{2}{\langle r^2 \rangle r_b} - \frac{\omega_c^2}{4(\gamma p c)^2} \frac{2 \langle r^2 \rangle}{r_b} - \frac{2 \langle r^2 \theta' \rangle^2}{r_b \langle r^2 \rangle}$$

$$+ \frac{2 \langle r^2 \theta'^2 \rangle}{r_b} + \frac{4 \langle r^2 \rangle \langle r'^2 \rangle - 4 \langle rr' \rangle^2}{r_b^3}$$

USING $r_b^2 \equiv 2 \langle r^2 \rangle$ & $r_b' = \frac{2 \langle rr' \rangle}{r_b}$

ENVELOPE EQUATION

$$\Rightarrow \boxed{r_b'' + \frac{\gamma'}{\beta^2 \gamma} r_b' + \frac{\gamma''}{2\beta^2 \gamma} r_b + \left(\frac{\omega_c}{2\gamma p c} \right)^2 r_b + \frac{-4 \langle p_\theta \rangle^2}{(\gamma m p c)^2 r_b^3} - \frac{\epsilon_r^2}{r_b^3} - \frac{Q}{r_b} = 0}$$

WHILE $\epsilon_r^2 = 4 (\langle r^2 \rangle \langle r'^2 \rangle - \langle rr' \rangle^2 + \langle r^2 \rangle \langle r^2 \theta'^2 \rangle - \langle r^2 \theta'^2 \rangle^2)$

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ENVELOPE EQUATION -- CONTINUED

$$r'' + \frac{\gamma'}{\beta^2 \gamma} r' + \frac{\gamma''}{2\beta^2 \gamma} r + \left(\frac{\omega_c}{2\gamma \mu c} \right)^2 r - \frac{4 \langle p_0 \rangle^2}{(\lambda m c)^2 r_b^3} - \frac{\epsilon_r^2}{r_b^3} - \frac{Q}{r_b} = 0$$

COMPARE WITH THE SINGLE PARTICLE PARAXIAL EQUATION:

$$r'' + \underbrace{\frac{\gamma'}{\beta^2 \gamma} r'}_{\text{INERTIAL}} + \underbrace{\frac{\gamma''}{2\beta^2 \gamma} r}_{\text{GR}} + \underbrace{\left(\frac{\omega_c}{2\gamma \mu c} \right)^2 r}_{V_0 B_z - \text{CENTRIFUGAL}} - \underbrace{\left(\frac{p_0}{\lambda m c} \right)^2 \frac{1}{r^3}}_{G-\text{MOLNIKOV}} - \underbrace{\frac{q}{r^3 m v_z^2} \frac{\lambda(r)}{2\pi \epsilon_0 r}}_{\text{GR} - V_0 B_z \text{ self field}} = 0$$

$$\epsilon_r^2 = 4 (\langle r^2 \rangle \langle r'^2 \rangle - \langle rr' \rangle^2 + \langle r^2 \rangle \langle r^2 \theta'^2 \rangle - \langle r^2 \theta'^2 \rangle)$$

NOTE THAT FOR AXISYMMETRIC TERMS ($\rho = \rho(r)$ ONLY)

$$\langle r^2 \rangle = \langle x^2 \rangle + \langle y^2 \rangle = 2 \langle x^2 \rangle$$

$$\Rightarrow 2 \langle rr' \rangle = 4 \langle xx' \rangle$$

$$\therefore \langle x'^2 \rangle + \langle y'^2 \rangle = 2 \langle x'^2 \rangle = \langle r'^2 \rangle + \langle r^2 \theta'^2 \rangle$$

$$\text{DEFINE } \epsilon_x^2 = 16 (\langle x^2 \rangle \langle x'^2 \rangle - \langle xx' \rangle^2)$$

$$\Rightarrow \boxed{\epsilon_r^2 = \epsilon_x^2 - 4 \langle r^2 \theta'^2 \rangle}$$

EXAMPLES OF
SYSTEMS WITH AXIAL SYMMETRY

- PERIODIC SOLENOIDS
- EINZEL LENSES
- CONTINUOUS FOCUSING

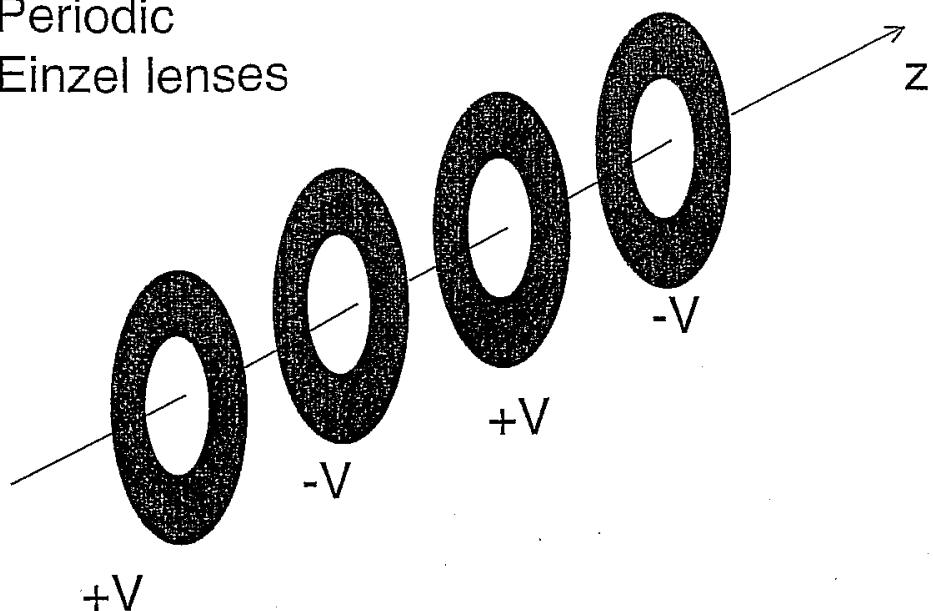
EXAMPLES OF
SYSTEMS WITHOUT AXIAL SYMMETRY

- ELECTRIC OR MAGNETIC QUADRUPOLE
- ⇒ USE CARTESIAN COORDINATES WITH
ELLITICAL SPATIAL CHARGE SYMMETRY

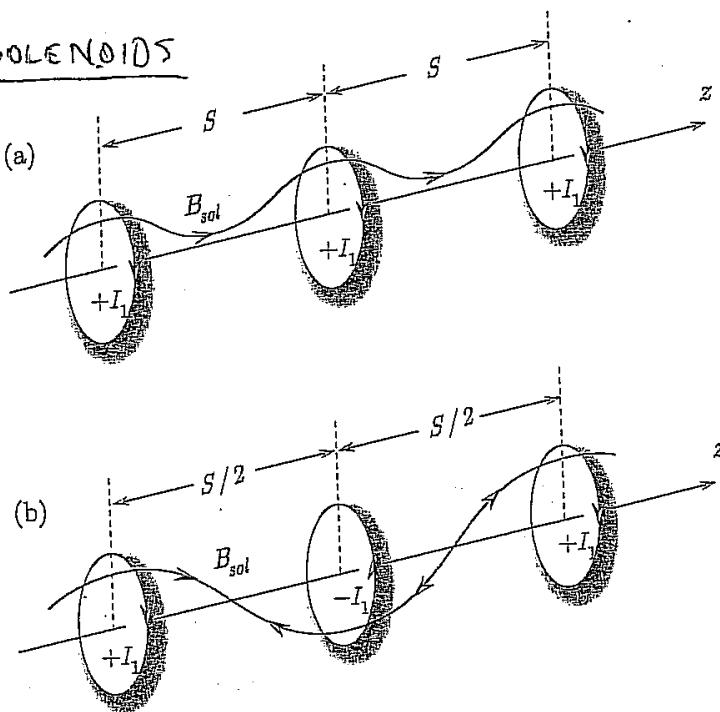
EXAMPLES OF AXISYMMETRIC SYSTEMS

(19)

Periodic Einzel lenses



PERIODIC SOLENOIDS



(FIGURE FROM
DAVIDSON & QIN
2003) p. 55

"PHYSICS OF
INTENSE CHARGE
PARTICLE BEAMS
IN HIGH ENERGY
ACCELERATORS"

Figure 3.2. Schematic of magnet sets producing a periodic focusing solenoidal field with axial periodicity length S . In Fig. 3.2 (a), successive coils are spaced by S and have the same current polarity $+I_1, +I_1, \dots$. In Fig. 3.2 (b), successive coils are spaced by $S/2$ and have alternating current polarities $+I_1, -I_1, +I_1, \dots$.

EXAMPLE OF NON-AXISYMMETRIC SYSTEM

54

Particle Orbits

3.2]

(20)

figure from
Davidson & Qin, 2003.

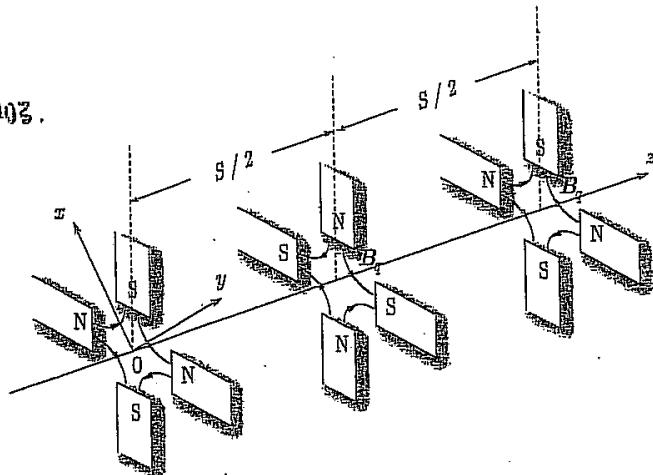


Figure 3.1. Schematic of magnet sets producing an alternating-gradient quadrupole field with axial periodicity length S .

NON-AXISYMMETRIC SYSTEM

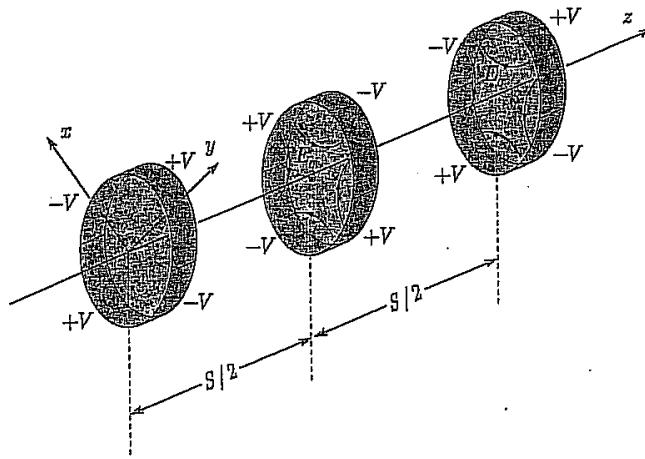


Figure 3.3. Schematic of conductor configuration with applied voltages producing an alternating-gradient quadrupole electric field with axial periodicity length S .

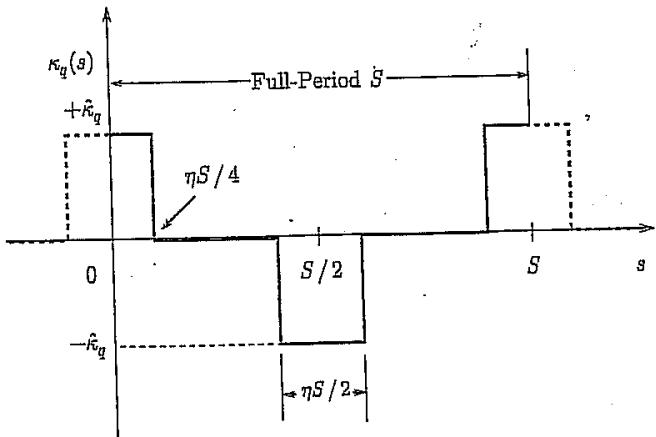


Figure 3.7. Alternating step-function model of a periodic quadrupole lattice with filling factor η for the lens elements. The figure shows a plot of the quadrupole coupling coefficient $\kappa_q(s)$ versus s for one full period (S) of the lattice. Such a configuration is often called a FODO transport lattice (acronym for focusing-off-defocusing-off).

FIGURES FROM DAVIDSON & QIN 2003

J. BARNARD

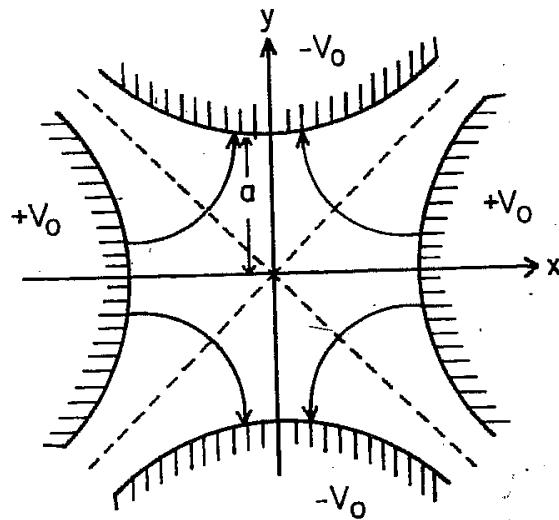
(22)

2 = BEAM OPTICS AND FOCUSING SYSTEMS WITHOUT SPACE CH

FROM
REISER, p. 112

$$E_x = -E'x$$

$$E_y = E'y$$



$$F_x = -qE'x$$

$$F_y = qE'y$$

ELECTROSTATIC
QUADS

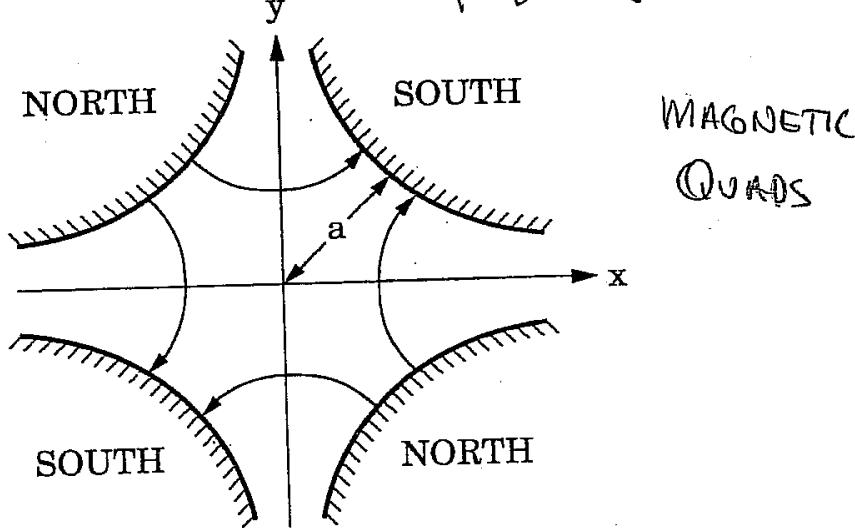
Figure 3.15. Electrodes and force lines in an electrostatic quadrupole.

$$B_x = B'y$$

$$B_y = B'x$$

$$F_x = -qv_z B'x$$

$$F_y = qv_x B'y$$



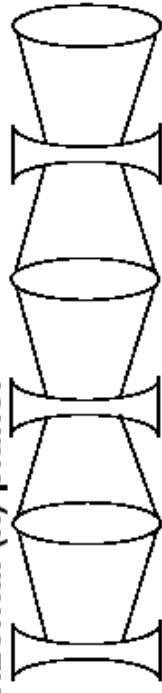
Heavy ion accelerators use alternating gradient quadrupoles to confine the beams

Space-charge forces and thermal forces act to expand beam

Quadrupoles (magnetic or electric):

- alternately provide inward then outward impulse
- focus in one plane and defocus in other
- act as linear lenses. (Force proportional to distance from axis).

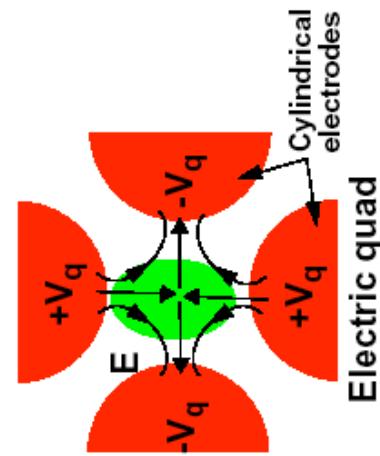
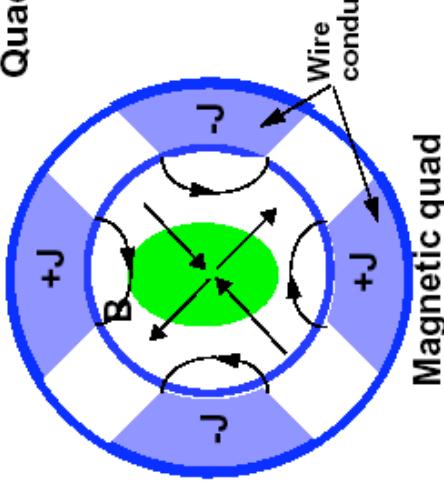
Horizontal (x) plane:



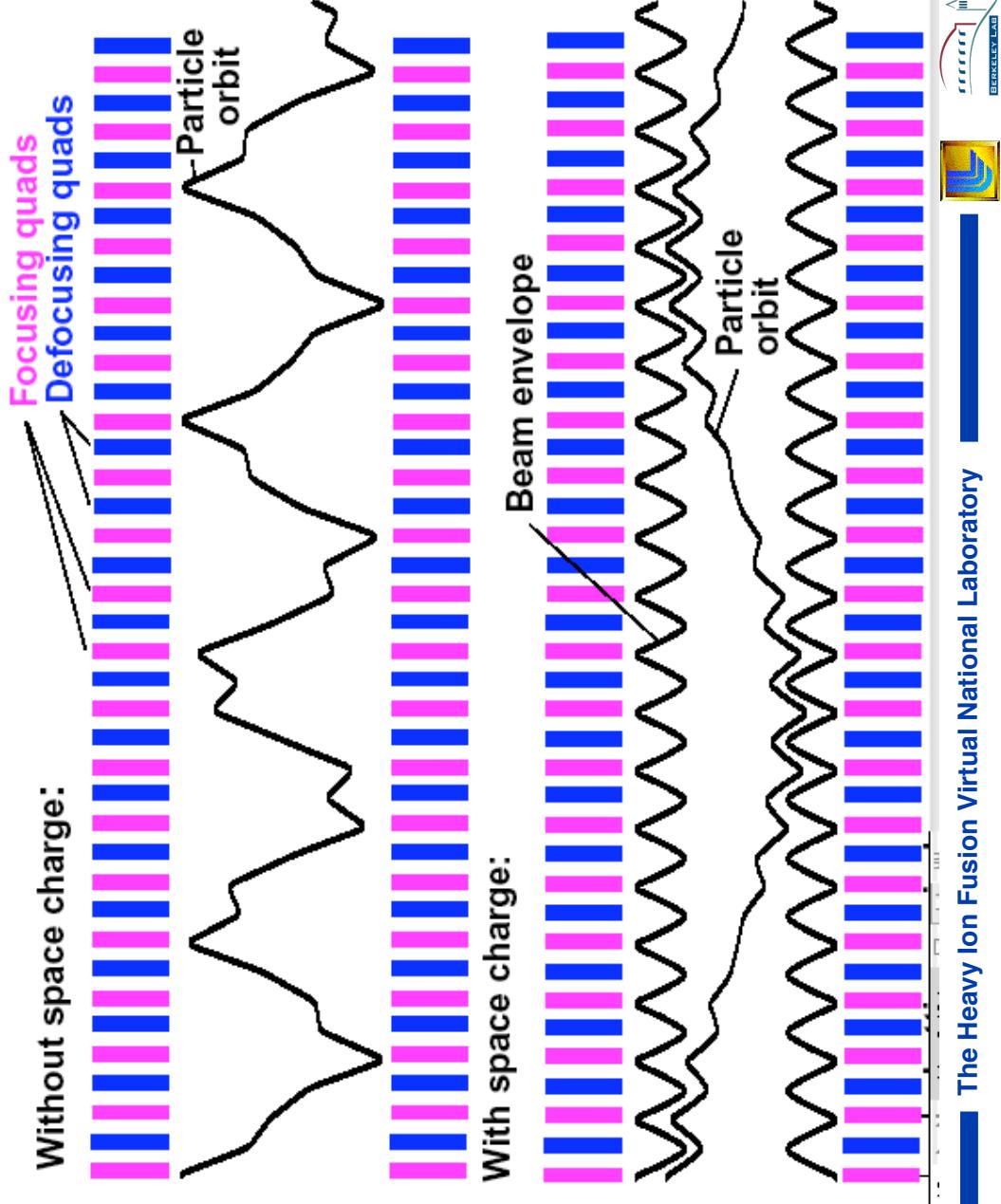
Vertical (y) plane:



Average displacement
is larger in focusing lenses
so the net effect is focusing.



Space charge reduces betatron phase advance



ENVELOPE EQUATIONS FOR NON-AXISYMMETRIC SYSTEMS

(25)

$$r_x^2 = 4 \langle x^2 \rangle \quad r_y^2 = 4 \langle y^2 \rangle$$

$$2r_x r_x' = 8 \langle xx' \rangle$$

$$v_x' = \frac{4 \langle xx' \rangle}{r_x}$$

$$\begin{aligned} r_x'' &= \frac{4 \langle xx'' \rangle}{r_x} + \frac{4 \langle x'^2 \rangle}{r_x} - \frac{4 \langle xx' \rangle}{r_x^2} r_x' \\ &= \frac{4 \langle xx'' \rangle}{r_x} + \frac{16 \langle x'^2 \rangle \langle x^2 \rangle}{r_x^3} - \frac{16 \langle xx' \rangle^2}{r_x^3} \end{aligned}$$

$$\text{DEFINE } \epsilon_x^2 = 16(\langle x^2 \rangle \langle x'^2 \rangle - \langle xx' \rangle^2)$$

$$\Rightarrow \boxed{r_x'' = \frac{4 \langle xx'' \rangle}{r_x} + \frac{\epsilon_x^2}{r_x^3}}$$

So how do we calculate $\langle xx'' \rangle$?

RETURN TO SINGLE PARTICLE EQUATION (IN CARTESIAN COORDINATES)

$$\frac{d}{dt} (\gamma m \dot{x}) = \gamma m \ddot{x} + \gamma m \dot{x} = q(E_x + \dot{y}B_z - \dot{z}B_y)$$

↓

x''

& similarly

y''

↓
QUADRUPOLE FOCUSING

S/ALT-CHARGE OF ELLIPTICAL BEAMS

TO BE CONTINUED ...

J. BANNARD

QUADRUPOLE FOCUSING

Now, relax radial symmetry:

For $\nabla \cdot \mathbf{E} = 0$ & $\nabla \times \mathbf{B} = 0$

EXPAND FIELD IN CYLINDRICAL "MULTIPOLES":

$$E_r, B_r = \sum_{n=1}^{\infty} f_n r^{n-1} \cos(n\theta)$$

$$E_\theta, B_\theta = \sum_{n=1}^{\infty} f_n r^{n-1} \sin(n\theta)$$

$$n=1 \Rightarrow \text{dipole} \quad \begin{cases} E_r = f_1 \cos\theta \\ E_\theta = f_1 \sin\theta \end{cases} \Rightarrow \begin{cases} E_x = f_1 \\ E_y = 0 \end{cases}$$

$$n=2 \Rightarrow \text{quadrupole} \quad \begin{cases} E_r = f_2 r \cos 2\theta \\ E_\theta = -f_2 r \sin 2\theta \end{cases} \Rightarrow \begin{cases} E_x = f_2 x \\ E_y = -f_2 y \end{cases}$$

NOTE: ABOVE EXPANSION IS VALID WHEN $E \text{ & } B \neq \text{function}(z)$.FOR MAGNETS OF FINITE AXIAL EXTENT, FOR EACH FUNDAMENTAL n-pole, A SET OF HIGHER ORDER MULTipoles WITH SAME AZIMUTHAL SYMMETRY ARE REQUIRED TO SATISFY $\oint \vec{B} \cdot d\vec{\ell} = 0$.

FOR EXAMPLE FOR A FUNDAMENTAL QUADRUPOLE THE FIELD MAY BE EXPANDED:

$$E_r = \sum_{v=0}^{\infty} f_{2,v}(z) [1+v] r^{1+2v} \cos[2\theta]$$

$$E_\theta = \sum_{v=0}^{\infty} -f_{2,v}(z) r^{1+2v} \sin[2\theta]$$

$$E_z = \sum_{v=0}^{\infty} \frac{1}{2} \frac{df_{2,v}}{dz} r^{2+2v} \cos 2\theta$$

$$\text{with } f_{2,v+1}(z) = \frac{-1}{4(v+1)(v+3)} \frac{d^2 f_{2,v}(z)}{dz^2}$$



$$E_x = E_r \cos\theta - E_\theta \sin\theta$$

$$E_y = E_r \sin\theta + E_\theta \cos\theta$$

SEE LUND, S. M. (1996)
FOR EXAMPLE. HIF with 96-
LNLS.